Appendix 2

Structural Proposal



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PROJECT:

HUNG HOM BAY RECLAMATION PHASE II, HUNG HOM (NORTH) FERRY PIER, HONG KONG

Structural Appraisal Report Apr 2024

Title	AP/RSE				
Name	Wong Shing Tsang (RSE 12/00)				
Signature					
Date	03 April 2024				

I. <u>Introduction</u>

This report presents a structural appraisal calculation for addition of a proposed sprinkler water tank and sprinkler pump room on the roof floor of Hung Hom (North) Ferry Pier, Hung Hom, Kowloon, Hong Kong.



II. <u>Relevance Regulations and Code of Practices for Checking</u>

The works shall be carried out in strict compliance with, but not limited to the following:

- Hong Kong Building (Construction) Regulation
- Code of Practice for the Structural Use of Steel –2011
- Code of Practice for Structural Use of Concrete 2013
- Code of Practice for Dead and Imposed Load 2011
- Code of Practice on Wind Effects in Hong Kong 2019

III. <u>Design Data</u>

1.1 Dead Load:

Reinforced Concrete Self-weight = 24.5 kN/m^3 ,

Water Density = 9.81kN/m³,

Sprinkler Water Tank Self-weight = 2150kg,

Sprinkler Pump Room Self-weight = 300kg.

1.2 Wind Pressure: Water Tank = 1.991kPa

Effective height = 13.65m, Qo,z = 2.08kPa, Cp = 1.1, Ss = 1.024, $L_{0.5p}$ = 10

IV. Existing Structural Data

- a). Concrete Grade of structural elements to be designed concrete mix with following minimum strength at 28 days and maximum size of aggregate 20mm:
 Column, wall, beam, slab and staircases 40MPa
- b). Concrete Cover:
 40mm above +4.000 Chart Datum (C.D.)
 60mm at or below +4.000 C.D.
 75mm bottom of pile cap unless otherwise specified.
- c). All reinforcement to comply with B.S. 4449.
- d). Existing Slab Thickness = 150mm

V. <u>Conclusion</u>

In conclusion, the proposed addition of water tanks on the roof is structurally feasible. Steel beams are proposed to transfer the extra load of the water tanks to the columns directly.

In general, the existing structures (columns and piles) are capable for supporting the new loading from the proposed water tanks.

Appendices

- Appendix A Structural Calculation
- Appendix B Drawings
- Appendix C Record Plan

Appendix A Structural Calculation

Loading

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=F	CALCULATIONS	Duie		
-1 -	O/LEGEL/HONG			001101
	Loading			
	Loading due to two new sprinkler water tanks and sprinkler	r pump room		
	(Assume Size = $7m \times 4m \times 3m$ (H) = $84m^3 \times 2$ tanks = 168	m ³ with capacit	v of not less than 110m ³	
	Assume Size = $1.5m \times 2.5m \times 1m (H) = 3.75m^3$			
	Loading due to New Steel Platform (Assume 8.3m x 5.3m)	x 3.9m(H)) and	New Steel Catwalk	
	(Assume Size = 3.35m x 0.6m)			
	Dead Load (D.L.), Live Load (L.L.) and Wind Load (W.L.) s	should be consi	dered are as follows:	
	D.L.: Include Self-Weight of Water Tank, steel works, etc.			
	Assume Dead Weight of New Steel Platform with Barrier R	ailing =	1.000 kPa	
	On Steel Platform, D.L. = 8.3m x 5.3m x 1kPa	=	43.990 kN	
	On Steel Catwalk, D.L. = 3.35m x 0.6m x 1kPa	=	2.010 kN	
	Self-weight of Water Tank, D.L. = 2 x 2150kg x 9.81ms ⁻² /1	= 000	42.183 kN	
	Self-weight of sprinkler pump room, D.L. = 300kg x 9.81ms	s ⁻² /1000 =	2.943 kN	
	L.L.: Imposed Load for Roof and Water Load			
	Imposed load for roof	=	2.000 kPa	
	On Steel Platform, L.L. = 8.3m x 5.3m x 2kPa	=	87.980 kN	
	On Steel Catwalk, L.L. = 3.35m x 0.6m x 2kPa	=	4.020 kN	
	Water Load			
	Case A) For the 110,000Litres (110m ³) water, 110m ³ x9.81	N/m ³ =	1079.1 kN	
	Case B) For the maximum 70% of the 168,000Litres (168n	n ³) water,		
	= (168x0.7)m ³ x9.81kN/m ³	=	1153.7 kN	
	W.L: Wind force acting on sprinkler water tank			
	Breadth of the sprinkler water tank	=	7.000 m	
	Height of the sprinkler water tank	=	3.000 m	
	Pressure coefficient (C _p)	=	1.100	
	Effective height (Z _e)	=	13.650 m	
	Design wind reference pressure (Q _{o,z})			
	$= 3.7 \times (13.65/500)^{0.16}$	=	2.080 kPa	
	Topography factor (S _t)	=	1.000	
	The wind directionality factor (S_{θ})	=	0.850	
	Design wind pressure (Q _z)			
	$= Q_{o,z} \times S_t \times S_{\theta} = 2.08 \times 1 \times 0.85$	=	1.768 kPa	
	Size of loaded area (L _{0.5p})			
	= 7+3	=	10.000 m	
	Size factor (S _s)			
	$= \exp(0.17 - 0.07 \times 10^{0.32})$	=	1.024	
	Design wind pressure (P)		4 004 1 5	
	$= Q_z \times C_p \times S_s = 1.68 \times 1.1 \times 1.024$	=	1.991 kPa	
	Chaolicad			

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Sectior	The existin	g loading	Rev.		Page:			
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REF.	CALCULATIONS							
	Loading Dead Load (D.L.), Live Load (D.L.: Include self-weight of the Finishes Service Self-weight of the slab L.L.: Imposed Load L.L. Total loading = 1.4D.L.+1.6L.L. For considering the wind load There are three storey at the H Hence, the loading add to the Load Area of Column C19 = 6 Hence, the loading adding to	L.L.) should be consider 2 slab, finishes, service 2 slab, finishes, service x 1.25 Pier, 4m, 7.3m and 10.6 column should be 3 tim .2m x 4.85m the column C19	red are as follows: = = = 5m level, es of the total load = =	0.600 kPa 0.600 kPa 10.000 kPa 5.000 kPa 23.68 kPa 29.60 kPa 88.800 kPa 30.070 m ² 2670.216 kN	(Critical)			
Calc.	Checked	Remarks			I			

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Sectior	Loading for the Beam B1 (203x203x	Rev.	Rev.				
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REF.	CAL	CULATIONS				0	DUTPUT
	Dead Load (D.L.) = 43.99 + 2.01 + 42.183 + 2.943 + 46.1kg/m x 6400/1000 x 9.81ms ⁻¹ + 24.5kN/m ³ x 60m ² x 150/1000 Live Load (L.L.) = 87.98 + 4.02 +1079.1 + 2kPa x 6 = 87.98 + 4.02 +1153.7 + 2kPa x 6	² /1000 0m ² (Case A) 0m ² (Case B)	= = =	314.520 1291.1 1365.7	kN kN kN		
	Wind Load (W.L.) = 1.991kPa x 7m x 3m			41.815	kN		
	$= (314.52 \pm 1291.1 \pm 41.815)/6.2$		_	265 715	kN/m		
	= (314.52 + 1365.7 + 41.815)/6.2	(Case B)	=	277.748	kN/m		
	Shear = (314.52 + 1291.1 + 41.815)/2 (Case A) = (314.52 + 1365.7 + 41.815)/2 (Case B)			823.718 861.018	kN kN		
	Moment Support moment	=	0.000	kNm			
	Mid-span momen = 265.715 x 6.2 >	(Case A)	=	1276.762	kNm		
	Mid-span momen = 277.748 x 6.2 >	: 6.2/8 (Case B)	=	1334.577	kNm		
Calc.							

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Section	Loading	for the Beam B1 (203x203x46kg/m	UC) (6200mm(L	_))	Rev.			Page:
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	Load Area of S	Steel Beams and Columns						
	Load Area of S	Steel Beam B1			=	21.235 m	2	
	Load Area of 0	Column C19			=	30.070 m	2	(Critical)
	The Loading o	f Existing Columns are as follows:						
		D.L.	L.L.	D.L.+L.L				
	C19)	5000kN	1520kN	6520kN				
	Original Desig Concrete Grac Concrete Cove Load Path of N (D.L. +L.L. +W (B19, B20, C1	n Data de = 40 MPa er of column = 40 mm New Steel Platform /.L.)>Steel Platform>New Steel B /.L.) C19, C20, D17, D19 and D20)>	Beams (B1)>E Existing Founda	xisting R.C. (Columns			
Calc.	Check	ed F	Remarks					

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Section	Existing column			Rev			Page.
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		-					
	For checking the Column C19						
	Area of Column C19			=	0.19635	m ²	
	Self-weight of the C19 $24.54 \text{ M}/\text{m}^3 + (0.40005 \text{m}^2 + 0.05 \text{m})$			_	21.000	LNI	
	= 24.5KN/M ⁻ X (0.19635M ⁻ X 6.65M)			=	31.990	KIN	
	The loading of the beam B1 (New)						
	= 277.748kN/m x 6.2m			=	1722.038	kN	
	The loading adding to the Column C19			=	2670.216	kN	
	Total load on the Column C19						
	= 2670.216 + 1722.038 + 31.99			=	4424,244	kN	
				<	6520	kN	O.K.
Calc.	Checked	Remarks	6				

Appendix B Drawings

1. ALL DIMENSIONS IN MILLIMETRES. ALL LEVELS REFER TO CHART DATUM (C.D.) AND IN MILLIMETRES. CONCRETE TO STRUCTURES TO BE OF GRADE 40 / 20 ALL REINFORCEMENT TO COMPLY WITH B.S.4449. CONCRETE COVER TO REINFORCEMENT TO BE 40mm UNLESS OTHERWISE SPECIFIED. 20
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 1 200 OF CONFID. MINIMUM LAP LENGTH FOR REINFORCEMENT OF HIGH YIELD TYPE 2 DEFORMED BARS TO BE 45 TIMES THE DIAMETER OF THE SMALLER LAPPED BAR UNLESS OTHERWISE SPECIFIED. 4 000 MINIMUM ANCHORAGE LENGTH FOR REINFORCEMENT OF HIGH YIELD TYPE 2 DEFORMED BARS TO BE 32 TIMES THE DIAMETER OF BAR UNLESS OTHERWISE SPECIFIED. A ALL EXTERNAL CONCRETE ARRISES TO BE 25×25mm CHAMFERED UNLESS OTHERWISE SPECIFIED. B - 10T10 - 75 - 150B Н -14T12-16-29-150T 7 -10T10-76-150T -14T12-31-44-150E 2-1710-01 TAN TABIAT DAR - 4110-100 -14710-61-74-1501 3/710-13 11T12-30-150T 24T10-8-150T 24T10-9-1508 24T10-13-1508 24T10-14-150T -4T 10-105 -4T10-90 -4T10-90 -2+23T 12 -82 - 150 TAB 4T10-88-300T(L SHAPE) 4T10-89-300B(L SHAPE) -11712-45-1508 4710-88-300T(L SHAPE) -2-5710-63-300 748 2+4710-90-300 TEB (ST. BAR - 2+4T10-91-94-300T&B (ST. BAR) - 4T 10 - 108 - 2+23T12-82-150 TE 1200 -2+5T10-83-300 TEE 3710-99-3007 181 TAB 900 VC C T 12 - 30 - 150T 0 AS CONSTRUCTED (B) PREPARED: (I.O.W.) T. N. TSUI NFT 749T10-12-300 4.93 (ENGINEER) M. C. LEE 2008 VD 29710-14-2 12T10-11-300T 13T10-11-300T D no. det 25T 10-12-1508 REVIBIC 2+4T10-102 1051-2 8-1508 10110-1 TAB 9110-12-300 T&B GA 300 2 2 4 G 0 denigned T. K. CHEUNG 200 17-9-87 2=4110-90-300 T & 8 (ST. BAR) 0 Y. M. LEUNG Keng 3-11-8 -TEB Y. M. LEUNG Chen 3-11-8 HAPE S 2-300 2+9T10-12-300 2+9T10-12-30 T48 T48 W. TSUI K 6-1-88 3 ++10 750 -++10 650 29710-14-200B - Longiely 14 - 1 - 88 13T10-11-300T 12T 10 - 11 - 300 T 12 T 10 - 10 - 300T 13T 10 - 10 н moment no. CV/87/08 NE_ 19T10-1-200T EA P. W. O. CV/87/08 19T10-1-200T -1 287 10-1-2007 200 26710-1-2001 28T10-1-200T die no. 9T 10 -2 - 200 B roject no. 228 CL Eg HUNG HOM BAY 7T10-3-300T 7T10-4-3008 RECLAMATION PHASE I 2 - 4T 10 - 90 - 300 T&B(ST. BAR) 4T10-90 4710-97-300T(L SHAPE) 4710-98-300B(L SHAPE) CONSTRUCTION OF 4T10-95-300T(L SHAPE) 4T10-95-3008(L SHAPE) -2+4T10-90-300TAB(ST. BAR) -2+4T10-5- 300TAB - 2- / 710 - 90 - 30074 8/ 57 FERRY PIERS AND STEEL BEAMS INSTANCED ON TOP OF ROOF COLUMN HEADS TO SUPPORT THE ADDITIONAL WATER TANKS В SEAWALL STAGE I A drewing title PIER B ---R. C. DETAILS OF ROOF SLAB MAIN ROOF SLAB (SHEET 1 OF 5) drawing no. -P 16093A 1:100 office PORT WORKS DIVISION CIVIL ENGINEERING OFFICE CIVIL ENGINEERING ITI SERVICES DEPARTMENT HONG KONG

Appendix C Record Plan





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- 1. ALL DIMENSIONS IN MILLIMETRES.
- 2. ALL LEVELS REFER TO CHART DATUM (C.D.) AND IN MILLIMETRES.
- 3. CONCRETE TO STRUCTURES TO BE OF GRADE 40/20.
- 4. ALL REINFORCEMENT TO COMPLY WITH
- 5. CONCRETE COVER TO REINFORCEMENT TO BE 40mm.
- 6. MINIMUM LAP LENGTH FOR REINFORCEMENT OF HIGH YIELD TYPE 2 DEFORMED BARS TO BE 45 TIMES THE DIAMETER OF THE SMALLER LAPPED BAR UNLESS OTHERWISE SPECIFIED.
- 7. MINIMUM ANCHORAGE LENGTH FOR REINFORCEMENT OF HIGH YIELD TYPE 2 DEFORMED BARS TO BE 32 TIMES THE DIAMETER OF BAR UNLESS OTHERWISE
- 8. ALL EXTERNAL CONCRETE ARRISES TO BE 25 x 25 mm CHAMFERED UNLESS OTHERWISE SPECIFIED.

AS CONSTRUCTED PREPARED: T. N. TSUI (I.O.W.) CERTIFIED: M. C. LEE Thes La (ENGINEER) description initial name date T. K. CHEUNG M 17-9-87 C.Y.LAI 12-10-87 ari C. Y. LAI Lai 14-10-87 6-1-88 W. TSUI 13-1-88 -Lopailly contract no. CV / 87/08 file no. P. W. O. CV / 87 / 08 project no. 228 CL HUNG HOM BAY RECLAMATION PHASE II CONSTRUCTION OF FERRY PIERS AND SEAWALL STAGE I PIER B----R. C. DETAILS OF COLUMNS (SHEET 1 OF 4) scale P16099A 1:25

PORT WORKS DIVISION CIVIL ENGINEERING OFFICE

> **CIVIL ENGINEERING** SERVICES DEPARTMENT HONG KONG

